

Přípravné výpočty stability alternátoru

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Parametry zařízení

$$U_n = 400$$

$$U_{nf} = \frac{U_n}{\sqrt{3}}$$

$$S_{ng} = 100$$

$$\cos(\varphi) = 0.8$$

$$P_{ng} = S_{ng} \cdot \cos(\varphi)$$

$$x_d = \frac{120}{100} \cdot \frac{U_n^2}{S_{ng}} \cdot i$$

$$x_d' = \frac{30}{100} \cdot \frac{U_n^2}{S_{ng}} \cdot i$$

`% Napeti`

`i=sqrt(-1)`

`Un=400`

`Unf=Un/sqrt(3)`

`% Generator`

`Sng=100`

`CosFi=0.8`

`Png=Sng*CosFi`

`Xd= (120/100) * (Un^2/Sng) * i`

`Xdc= (30/100) * (Un^2/Sng) * i`

Parametry zařízení

$$S_{nt1} = 100$$

$$u_{kt1} = 10$$

$$X_{t1} = \frac{U_{kt1}}{100} \cdot \frac{U_n^2}{S_{nt1}} \cdot i$$

$$delka = 50$$

$$X_{v1} = delka \cdot 0.3 \cdot i \frac{U_n^2}{110^2}$$

$$Xv = \frac{Xv1}{2}$$

`% Transformator T1`

`Snt1=100`

`Ukt1=10`

`Xt1=(Ukt1/100) * (Un^2/Snt1) * i`

`% Vedeni`

`delka=50`

`Xv1=delka*0.3*i/110^2*Un^2`

`Xv=Xv1/2`

Parametry zařízení

$$S_{nt2} = 100$$

$$u_{kt2} = 10$$

$$X_{t2} = \frac{U_{kt2}}{100} \cdot \frac{U_n^2}{S_{nt2}} \cdot i$$

$$S_k = 10000$$

$$C = 1$$

$$X_s = C \cdot \frac{U_n^2}{S_k} \cdot i$$

`% Transformator T2`

`Snt2=100`

`Ukt2=10`

`Xt2=(Ukt2/100) * (Un^2/Snt2) * i`

`% Sit`

`Sk=10000`

`KoefC=1`

`Xs=KoefC * (Un^2/Sk) * i`

Předporuchový stav

$$P_{ng0} = 1.00 \cdot P_{ng}$$

$$P_t = P_{ng0}$$

$$\vartheta = \frac{75}{180} \pi$$

$$\vartheta' = \vartheta$$

$$X_{suma} = |X_d + X_{t1} + X_v + X_{t2} + X_s|$$

$$X_{suma}' = |X_d' + X_{t1} + X_v + X_{t2} + X_s|$$

% Vypocet predporuchoveho
stavu, pocatecni zatizeni
100%

% Zvolit zatezny uhel

Png0=1.00*Png

Pt=Png0

Theta=75/180*pi

Thetac=Theta

% Celkova vazebni reaktance

Xsuma =abs(Xd +Xt1+Xv+Xt2+Xs)

Xsumac=abs(Xdc+Xt1+Xv+Xt2+Xs)

Předporuchový stav

$$E = \frac{P_{ng0}}{3 \cdot U_{nf} \cdot \sin(\vartheta)} X_{suma}$$

% Vypocet potrebného nabuzení E a E'

$$E = Png0/3/Unf*Xsuma/sin(Theta)$$

$$E' = \frac{P_{ng0}}{3 \cdot U_{nf} \cdot \sin(\vartheta)} X_{suma}'$$

$$Ec = Png0/3/Unf*Xsumac/sin(Theta)$$

$$P_{gkontrola} = 3 \frac{E \cdot U_{nf}}{X_{suma}} \sin(\vartheta)$$

$$Pgkontrola = 3 * E * Unf / Xsuma * sin(Theta)$$

$$P_{gkontrola}' = 3 \frac{E' \cdot U_{nf}}{X_{suma}'} \sin(\vartheta)$$

$$Pgckontrola = 3 * Ec * Unf / Xsumac * sin(Thetac)$$

Zkrat v polovině vedení

% Zkrat v polovine vedeni Xv1

$$X_a = \frac{X_{v1} \frac{X_{v1}}{2}}{X_{v1} + \frac{X_{v1}}{2} + \frac{X_{v1}}{2}}$$

$$X_b = \frac{X_{v1} \frac{X_{v1}}{2}}{X_{v1} + \frac{X_{v1}}{2} + \frac{X_{v1}}{2}}$$

$$X_c = \frac{\frac{X_{v1}}{2} \cdot \frac{X_{v1}}{2}}{X_{v1} + \frac{X_{v1}}{2} + \frac{X_{v1}}{2}}$$

% Nahrada trojuhelnika hvezdou

$$X_a = X_{v1} * X_{v1} / 2 / (X_{v1} + X_{v1} / 2 + X_{v1} / 2)$$

$$X_b = X_{v1} * X_{v1} / 2 / (X_{v1} + X_{v1} / 2 + X_{v1} / 2)$$

$$X_c = X_{v1} / 2 * X_{v1} / 2 / (X_{v1} + X_{v1} / 2 + X_{v1} / 2)$$

$$X_l = X_{d'} + X_{t1} + X_a$$

$$X_r = X_b + X_{t2} + X_s$$

$$X_{sumazkrat} = X_l + X_r + \frac{X_l \cdot X_r}{X_c}$$

$$X_l = X_{dc} + X_{t1} + X_a$$

$$X_r = X_b + X_{t2} + X_s$$

$$X_{sumazkrat} = \text{abs}(X_l + X_r + X_l * X_r / X_c)$$

Odpojení poruchy

$$X_{sumaodpojeno} = |i \cdot X_{suma} - X_v + X_{v1}|$$

$$X_{sumaodpojeno2} = |X_{dc} + X_{t1} + X_{v1} + X_{t2} + X_s|$$

$$P_{max1} = 3 \frac{Ec \cdot Unf}{X_{suma}'}$$
$$P_{max2} = 3 \frac{Ec \cdot Unf}{X_{sumazkrat}}$$
$$P_{max3} = 3 \frac{Ec \cdot Unf}{X_{sumaodpojeno}}$$

$$Y_{12} = \frac{1}{X_{suma}'}$$
$$Y_{12zkrat} = \frac{1}{X_{sumazkrat}}$$
$$Y_{12odpojeno} = \frac{1}{X_{sumaodpojeno}}$$

% Odpojeni poruchy

```
Xsumaodpojeno=
    abs(i*Xsumac -Xv + Xv1)
```

```
Xsumaodpojeno2=
    abs(Xdc + Xt1 + Xv1 + Xt2 + Xs)
```

% Konecne alternativy maximalnich
dodavanych cinnych vykonu

```
Pmax1=3*Ec*Unf/Xsumac
```

```
Pmax2=3*Ec*Unf/Xsumazkrat
```

```
Pmax3=3*Ec*Unf/Xsumaodpojeno
```

% Kontrolni admittance

```
Y12=      1/Xsumac
```

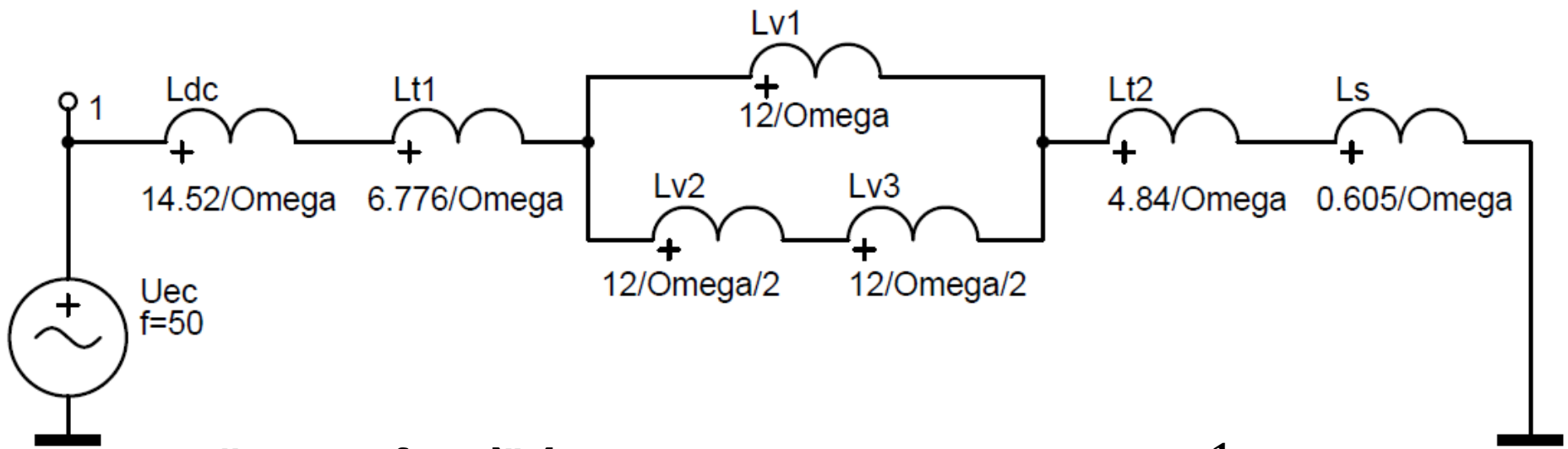
```
Y12zkrat= 1/Xsumazkrat
```

```
Y12odpojeno=1/Xsumaodpojeno
```


Předporuchový stav

$$X_{suma} = |X_d + X_{t1} + X_v + X_{t2} + X_s|$$

$$X_{suma}' = |X_d' + X_{t1} + X_v + X_{t2} + X_s|$$



| X ... | freq [Hz] |
|-------|-----------|
| 1 ... | MOD.I.Ldc |
| 2 ... | DEG.I.Ldc |
| 3 ... | MOD.I.Ls |
| 4 ... | DEG.I.Ls |

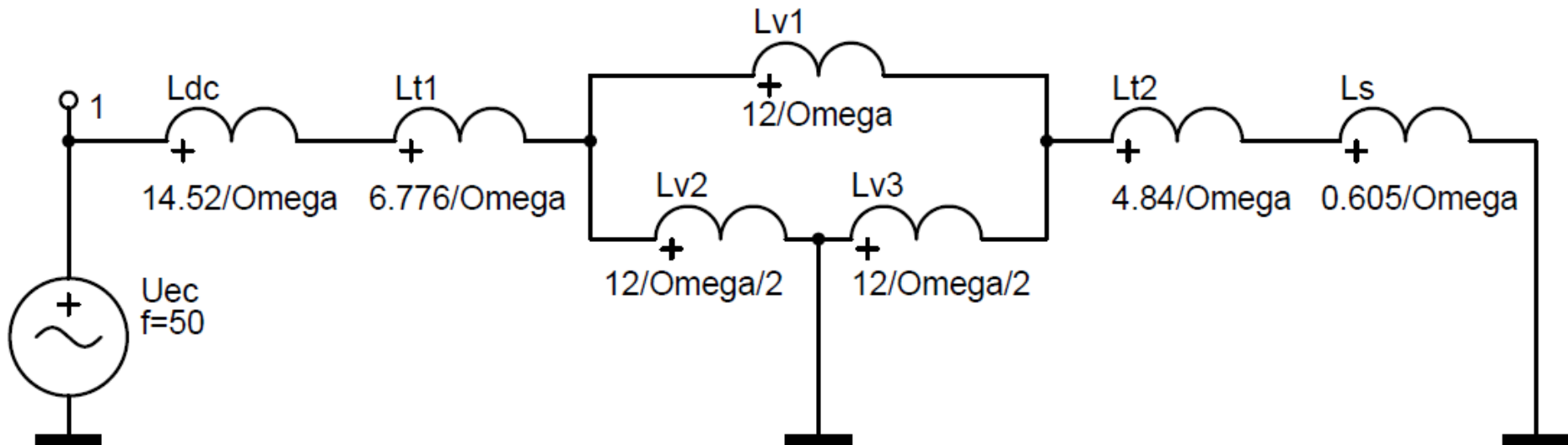
$$Y_{12} = \frac{1}{X_{suma}'}$$



| X | 1 | 2 | 3 | 4 |
|---------------|---------------|---------------|---------------|---------------|
| 5.000000e+001 | 3.054274e-002 | 2.700000e+002 | 3.054274e-002 | 2.700000e+002 |

Zkrat v polovině vedení

$$X_{sumazkrat} = X_l + X_r + \frac{X_l \cdot X_r}{X_c}$$



| X ... | freq [Hz] |
|-------|-----------|
| 1 ... | MOD.I.Ldc |
| 2 ... | DEG.I.Ldc |
| 3 ... | MOD.I.Ls |
| 4 ... | DEG.I.Ls |

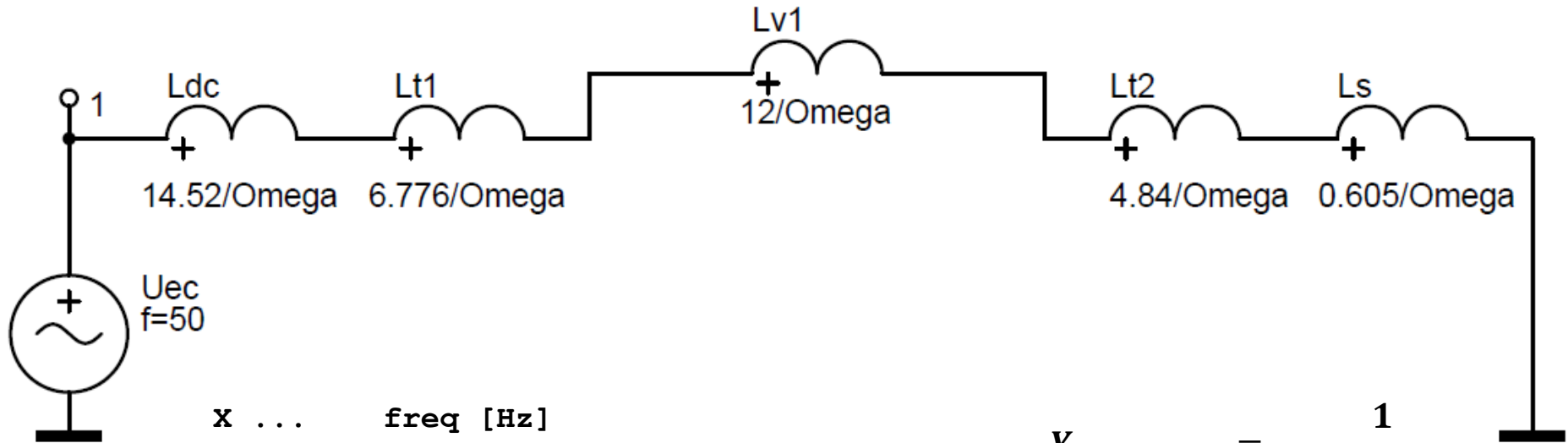
$$Y_{12zkrat} = \frac{1}{X_{sumazkrat}}$$



| X | 1 | 2 | 3 | 4 |
|---------------|---------------|---------------|---------------|---------------|
| 5.000000e+001 | 3.910870e-002 | 2.700000e+002 | 5.898749e-003 | 2.700000e+002 |

Odpojení poruchy

$$X_{sumaodpojeno} = |X_{dc} + X_{t1} + X_{v1} + X_{t2} + X_s|$$



| X ... | freq [Hz] |
|-------|-----------|
| 1 ... | MOD.I.Ldc |
| 2 ... | DEG.I.Ldc |
| 3 ... | MOD.I.Ls |
| 4 ... | DEG.I.Ls |

$$Y_{12odpojeno} = \frac{1}{X_{sumaodpojeno}}$$



| X | 1 | 2 | 3 | 4 |
|---------------|---------------|---------------|---------------|---------------|
| 5.000000e+001 | 2.581245e-002 | 2.700000e+002 | 2.581245e-002 | 2.700000e+002 |